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## Universality of oscillatory instabilities in fluid mechanical systems

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**PAPER****Universality of oscillatory instabilities in fluid mechanical systems**Vladimir García-Morales<sup>1</sup>, Shruti Tandon<sup>2,3</sup>, Jürgen Kurths<sup>4,\*</sup> and R I Sujith<sup>2,3</sup><sup>1</sup> Departament de Física de la Terra i Termodinàmica, Universitat de València, E-46100 Burjassot, Spain<sup>2</sup> Department of Aerospace Engineering, Indian Institute of Technology Madras, Chennai 600036, India<sup>3</sup> Centre for Excellence for studying Critical Transitions in Complex Systems, Indian Institute of Technology Madras, Chennai 600036, India<sup>4</sup> Potsdam Institute for Climate Impact Research, 14473 Potsdam, Germany

\* Author to whom any correspondence should be addressed.

E-mail: [Juergen.Kurths@pik-potsdam.de](mailto:Juergen.Kurths@pik-potsdam.de)**Keywords:** oscillatory instability, complex Ginzburg–Landau equation, universal scaling laws, turbulent fluid and thermo-fluid systems**RECEIVED**  
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Oscillatory instability emerges amidst turbulent states in experiments in various turbulent fluid and thermo-fluid systems such as aero-acoustic, thermoacoustic and aeroelastic systems. For the time series of the relevant dynamic variable at the onset of the oscillatory instability, universal scaling behaviors have been discovered in experiments via the Hurst exponent and certain spectral measures. By means of a center manifold reduction, the spatiotemporal dynamics of these real systems can be mapped to a complex Ginzburg–Landau equation with a linear global coupling. In this work, we show that this model is able to capture the universal behaviors of the route to oscillatory instability, elucidating it as a transition from defect to phase turbulence mediated by the global coupling.

**1. Introduction**

Spatially extended ensembles of globally coupled nonlinear oscillators exhibit a wide variety of spatiotemporal patterns ranging from incoherence to uniform oscillations [1]. For example, in certain surface chemical reactions, global coupling is produced through mechanical interactions with the gas phase [2, 3]. Global coupling can lead to the emergence of synchronous behavior out of turbulence and the formation of a number of coherent structures in ensembles of both identical and non-identical oscillators [3–10].

Turbulent aero-acoustic [11], thermoacoustic [12] and aeroelastic systems [13] can be viewed as paradigmatic spatially extended ensembles of globally coupled nonlinear oscillators. In all these systems, the behavior of an averaged dynamic variable reflects self-organization in the microscopic degrees of freedom leading to global periodic oscillations emerging out of turbulent states. The relevant dynamic variable is the acoustic pressure in aero-acoustic and thermoacoustic systems, and the strain experienced by the cantilever in aeroelastic systems. A transition to a state, termed *oscillatory instability* (OI), occurs in the time series of this variable from low-amplitude aperiodic oscillations to high-amplitude periodic ones [14, 15]. As the control parameter of the turbulent flow (the Reynolds number  $Re$ ) is varied in experiments, bursts of periodic oscillations begin to emerge amidst chaotic fluctuations. This alternating periodic and aperiodic behavior, termed as intermittency, has been reported in turbulent aero-acoustic [16], aeroelastic [17] and thermoacoustic systems [18]. The epochs of periodic dynamics occurring amidst aperiodic fluctuations increase as OI is approached [15].

Recently, experiments have established that the relevant variable of the OI exhibits power law scaling behavior via the Hurst exponent [15] and a spectral measure (moment of the power spectrum) [15] during the emergence of order. Strikingly, the power law scaling exponents are universally same across different turbulent fluid and thermo-fluid systems. Here, we propose a novel perspective where the relevant variable is viewed as a spatial average of an order parameter obtained by reducing the original dynamics of the real fluid mechanical systems to an appropriate amplitude equation of a complex Ginzburg–Landau type. We show that, indeed, the cubic complex Ginzburg–Landau equation with a global linear coupling is able to capture the emergence of OI along with the universal scaling behaviors found in experiments.

In general, normal forms and perturbation theory, provide a convenient mathematical framework to get insight in otherwise mathematically untractable problems, as the study of multiple-soliton solutions in spatially extended systems [19], the derivation of exact analytical results for incompressible magnetohydrodynamic plasma turbulence [20] or the study of bubble interactions in fluidized granular media [21]. Since the pioneering works by Newell and Whitehead [22] and Kuramoto [23], the cubic-quintic Ginzburg–Landau equation is known to arise as a center manifold reduction of the Navier–Stokes equations that describe turbulent fluids at the Rayleigh–Bernard instability. The complex Ginzburg–Landau equation was later modified to account for the global coupling created by the pressure in chemical reaction tanks [1–3] and for the global coupling created by the electric current in (photo)electrochemical systems [5–7]. In the present work we consider a novel modification of the Ginzburg–Landau equation, by allowing the parameters of the local dynamics to be influenced by the global coupling at first order in a perturbation series expansion. The motivation for these modifications is to capture most prominent features of the OI that have been very recently observed in fluid mechanical systems.

OIs emerge from turbulent states due to internal nonlinear interactions [24]. For example, flame dynamics, acoustics and hydrodynamics are strongly coupled inside thermoacoustic systems, as found in gas turbines (for power-producing, aeronautical, and marine applications) [25] and rocket engines [26]. A positive feedback develops between the acoustic field and the heat release rate oscillations leading to high-amplitude self-sustained periodic oscillations that are catastrophic to these engineering systems. Similarly, the OI in aero-acoustic systems arises due to the coupling between the acoustic field and the vortex shedding in the flow within a confinement [24]. Such oscillatory dynamics has been studied in various aero-acoustic applications, such as driven cavities, jet noise, pipe whistling, and gas pipe networks [27]. Finally, the OI in aeroelastic systems occurs due to the interaction between the flow field and the structural elements of the system [24]. A classic example is the collapse of the Tacoma bridge in 1940 due to violent oscillations [28].

Previous models developed to explain the emergence of OI are phenomenological and have successfully reproduced experiment signals observed in thermoacoustic systems qualitatively. Matveev and Culick [29], and Seshadri *et al* [30] have discussed a model where vortex shedding times are dependent on acoustic field perturbations in a dump combustor. This model, referred to as the kicked oscillator model, is a reduced order model that explains the hydrodynamic and acoustic field coupling. The model was able to replicate the occurrence of intermittency enroute to OI. Similarly, Noiray [31], and Tandon *et al* [32] have discussed a model where linearised non-dimensional energy and momentum equations are used to model the acoustic field along with a nonlinear source term to model the heat released due to combustion. This source term is assumed to be of the subcritical or supercritical normal form. Indeed these models are also able to reproduce distinct intermittency signals during transition from aperiodic to periodic dynamics, similar to those observed in laboratory scale combustion systems. However, in the said models, the universal scaling of Hurst exponent and amplitude of acoustic pressure was not observed.

In this work, we formulate a mathematical model (discussed in section 2) that is able to capture the universality observed in the transition to OI through experiments in various fluid mechanical and thermo-fluid systems, reproducing both scaling laws of the amplitude of the dominant mode with the Hurst exponent and with the spectral measure (discussed in section 3). Thus, the benefit of using our mathematical model is that, we are able to replicate the qualitative experimental features observed in several fluid systems exhibiting OI as well as able to capture quantitatively the route to OI by varying a single global coupling parameter.

## 2. Model and computational details

We introduce a globally coupled Complex–Ginzburg Landau equation (GCGLE) to model the turbulent flow and nonlinear interactions in complex turbulent fluid systems. Our model can be understood as arising from a center manifold reduction of the original dynamics (which is a vector space that for example in thermoacoustic systems, consists of combustion, acoustic and hydrodynamic subspaces that are interdependent due to nonlinear interactions) leading to the spatiotemporal dynamics of an oscillatory field. The global coupling term captures the average strength of interactions between subsystems in a turbulent fluid and thermo-fluid system.

The only free parameter of our theory is the global coupling strength  $\gamma$ . We assume that variations in  $Re$  have an impact on  $\gamma$  and on the parameters governing the local dynamics of the oscillators through their dependence on  $\gamma$ . Our model is a GCGLE [1–3] of the form

$$\partial_t W = W + (1 + ic_1(\gamma)) \partial_x^2 W - (1 + ic_2(\gamma)) |W|^2 W + \gamma (W - \langle W \rangle). \quad (1)$$

This dimensionless equation describes the spatiotemporal evolution (dimensionless space  $x$  and time  $t$ ) of a complex order parameter  $W(x, t)$  characterizing a 1D spatially extended array of diffusively and globally coupled nonlinear oscillators past a supercritical Hopf bifurcation. The term  $\gamma(W - \langle W \rangle)$  represents the deviation between the local oscillators and the global average dynamics  $\langle W \rangle$ , where the brackets  $\langle \dots \rangle$  denote spatial averages. The parameter  $\gamma$  is the strength of the global coupling and can be either desynchronizing ( $\gamma < 0$ ) or synchronizing ( $\gamma > 0$ ). For example,  $\gamma$  represents the coupling of the global acoustic field with the hydrodynamic and combustion subsystems in a turbulent thermoacoustic system. Further, in such systems, the underlying turbulent hydrodynamic and heat release rate fluctuations introduce diffusive coupling and nonlinearities which are respectively modeled by the terms  $(1 + ic_1)\partial_x^2 W$  and  $-(1 + ic_2)|W|^2 W$  in equation (1), respectively. The real-valued functions  $c_1(\gamma)$  and  $c_2(\gamma)$  can be obtained from the oscillatory dynamics of any specific system by means of a center manifold reduction [4, 23, 33]. They can both be expressed as a power series of  $\gamma$  as

$$c_1(\gamma) = \sum_{k=0}^{\infty} c_1^{(k)} \gamma^k \approx c_1^{(0)} + c_1^{(1)} \gamma \quad (2)$$

$$c_2(\gamma) = \sum_{k=0}^{\infty} c_2^{(k)} \gamma^k \approx c_2^{(0)} + c_2^{(1)} \gamma. \quad (3)$$

The truncation of the above series to first order in  $\gamma$  is justified by the fact that  $\gamma$  is small. This warrants that equation (1) above can be derived from a center manifold reduction of the original dynamics [5]. Here, we shall consider  $-0.01 \leq \gamma \leq 0.0038$ . The values of the parameters  $c_i^{(j)}$ ,  $i = 1, 2$ ,  $j = 0, 1$  are fixed in all simulations to  $c_1^{(0)} = 8.25$ ,  $c_1^{(1)} = -798.95$ ,  $c_2^{(0)} = -0.75$ ,  $c_2^{(1)} = 51.05$ . Computations show that higher order contributions are negligible and, therefore, the corresponding coefficients of higher powers in  $\gamma$  are taken to be identically zero in order to reduce the number of parameters in the fitting of the theoretical curves. The exhaustive search leading to these values is guided by the fact that when  $\gamma = 0$ , the system is to be found in a defect turbulent state (combustion noise) and, therefore,  $1 + c_1^{(0)} c_2^{(0)} \ll 0$ , i.e. the system is found deep in the Benjamin–Feir (BF) unstable regime. As  $\gamma > 0$ , the inequality  $1 + c_1(\gamma)c_2(\gamma) < 0$  is not so strong because parameters  $c_1$  and  $c_2$  governing the local dynamics are driven by the global coupling to a situation where the uniform oscillation is gradually stabilized and, therefore, closer to the BF line.

Let  $p(t)$  denote the pressure fluctuations in aero-acoustic and thermoacoustic systems or the strain experienced by the cantilever in aeroelastic systems. We model  $p(t)$ , regardless of the specific system under consideration, as

$$p(t) = \frac{\lambda}{L} \int_0^L \text{Re}W(x, t) dx = \lambda \langle \text{Re}W \rangle \quad (4)$$

where  $\lambda$  is a constant,  $L$  is the (dimensionless) system size and  $\text{Re}W(x, t)$  denotes the real part of  $W(x, t)$ . We fix  $L = 100$  and  $\lambda = 0.83$  kPa in all simulations. The value of  $L$  is chosen so that the system is macroscopic and the spatial average is robust. The value of  $\lambda$  is obtained from fitting the amplitude of  $p(t)$  when all oscillators are synchronized [15]. In brief, since  $\text{Re}W$  directly models the experimental spatiotemporal dynamics, the relevant dynamical variable  $p(t)$  is merely proportional to the spatial average  $\langle \text{Re}W \rangle$ . (The imaginary part of the order parameter,  $\text{Im}W(x, t)$ , corresponds to the Hilbert transform of the experimental spatiotemporal dynamics [34].)

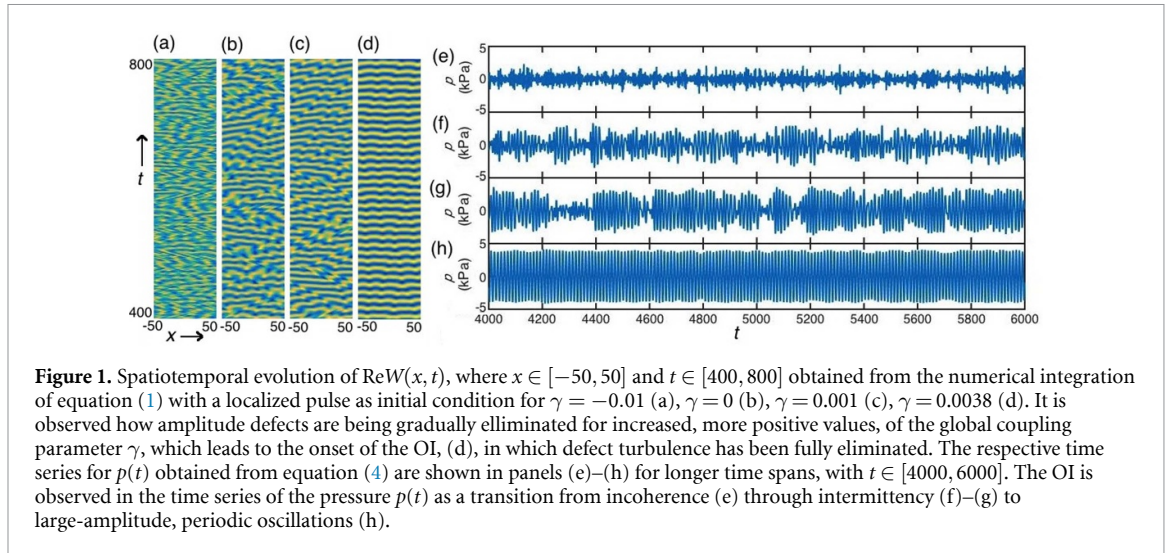
By applying periodic boundary conditions, the general solution of equation (1) can be written as

$$W(x, t) = \sum_{n=-\infty}^{\infty} W_n(t) e^{i2\pi nx/L}. \quad (5)$$

By replacing this general solution in equation (1) we find for the coefficients  $W_n(t)$  that

$$\dot{W}_n = \left[ 1 + \gamma(1 - \delta_{n0}) - (1 + ic_1) \left( \frac{2\pi n}{L} \right)^2 \right] W_n - (1 + ic_2) \sum_{j-k+l=n} W_j \tilde{W}_k W_l \quad (6)$$

where  $\delta_{n0} = 1$  if  $n = 0$  and  $\delta_{n0} = 0$  otherwise. Here the tilde denotes complex conjugation and the sum runs over all integer values for  $j$ ,  $k$  and  $l$  such that  $j - k + l = n$ . The sum is truncated for a number  $N = 512$  of Fourier modes and equation (6) is numerically solved by means of the ETD2K exponential time-stepping algorithm of Mathews and Cox [35]. The solution for  $W(x, t)$  is then obtained from equation (5), and  $p(t)$  is calculated from equation (4).



**Figure 1.** Spatiotemporal evolution of  $\text{Re}W(x, t)$ , where  $x \in [-50, 50]$  and  $t \in [400, 800]$  obtained from the numerical integration of equation (1) with a localized pulse as initial condition for  $\gamma = -0.01$  (a),  $\gamma = 0$  (b),  $\gamma = 0.001$  (c),  $\gamma = 0.0038$  (d). It is observed how amplitude defects are being gradually eliminated for increased, more positive values, of the global coupling parameter  $\gamma$ , which leads to the onset of the OI, (d), in which defect turbulence has been fully eliminated. The respective time series for  $p(t)$  obtained from equation (4) are shown in panels (e)–(h) for longer time spans, with  $t \in [4000, 6000]$ . The OI is observed in the time series of the pressure  $p(t)$  as a transition from incoherence (e) through intermittency (f)–(g) to large-amplitude, periodic oscillations (h).

### 3. Results

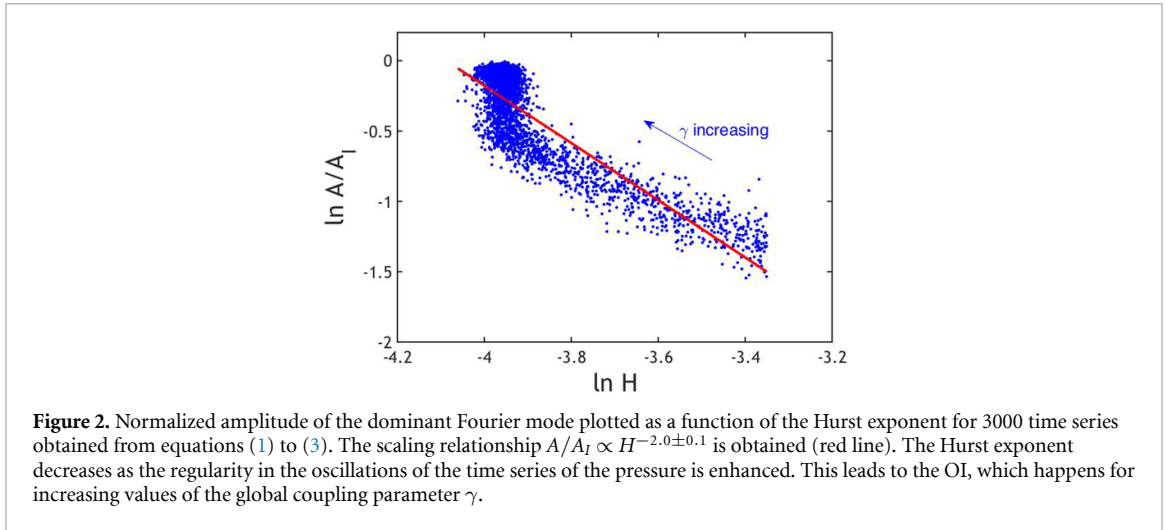
Oscillatory instability emerges when a fluctuation drives the system to self-sustained dynamics due to the self-organised feedback interactions within the system. In experiments, as the flow control parameter (Re) is increased, the strength of nonlinear interactions increases and governs the dynamics. To model such increase in nonlinear interactions, here, we increase the global coupling parameter of the GCGLE, changing it from  $\gamma < 0$  to  $> 0$ , while a local pulse perturbation simulates the initial fluctuation. Clearly, the GCGLE gives rise to intermittent periodic and self-sustained periodic oscillations for  $\gamma > 0$  and chaotic dynamics for  $\gamma < 0$ .

In figures 1(a)–(d), the spatiotemporal evolution of  $\text{Re}W(x, t)$ , for a localized pulse as initial condition, is shown for increasing values of  $\gamma$ : we have  $\gamma = -0.01$  (a),  $\gamma = 0$  (b),  $\gamma = 0.001$  (c),  $\gamma = 0.0038$  (d). The respective time series for  $p(t)$  are shown in panels (e)–(h) for longer time spans. For  $\gamma = 0$ , from equations (2) and (3) we have  $c_1 = c_1^{(0)} = 8.25$  and  $c_2 = c_2^{(0)} = -0.75$ . Since  $c_1 c_2 = -6.1875 < -1$ , when  $\gamma = 0$  the system is found in a state deep beyond the BF line, where the uniform oscillation is unstable to long wavelength perturbations. Indeed, the system exhibits *defect turbulence*: the presence of defects, i.e. those  $(x, t)$  pairs where  $|W(x, t)| = 0$ , causes discontinuities in the lines of constant phase yielding an irregular spatiotemporal pattern where the oscillators are incoherent, see figure 1(b). Now, if  $\gamma < 0$ , as in figure 1(a) where  $\gamma = -0.01$ , the density of defects is even higher because the coupling is de-synchronizing. On the contrary, if the global coupling is positive, as in figures 1(c) and (d), defect turbulence tends to be suppressed. The density of defects diminishes until they are fully suppressed and only slight phase modulations remain, the lines of constant phase being continuous everywhere and the oscillators being synchronous.

The impact of this spatiotemporal behavior on  $p(t)$  now becomes qualitatively clear. In figures 1(e)–(h),  $p(t)$  is shown for different values of  $\gamma$ . We note that  $0 \leq |p(t)| \leq p_{\max}$ , where the upper bound  $p_{\max} = \lambda N/L = 4267$  Pa is reached only when all oscillators are synchronous, all constructively contributing to the spatial average in equation (4). The lower bound  $|p| = 0$  is obtained in the extreme case in which the density of defects is so high that the oscillators are fully incoherent so that their spatial average vanishes. This situation is approached in figure 1(e), where  $\gamma = -0.01$ .

As  $\gamma$  is increased to  $\gamma = 0$  in figure 1(f) and  $\gamma = 0.001$  in figure 1(g), the time series tends to become intermittent owing to a gradual elimination of the defects in the spatiotemporal dynamics of oscillators. Hence, there are epochs when a majority of the oscillators are synchronized, while at other epochs they are desynchronized. This leads to bursts of periodic behavior interspersed between intervals of low-amplitude aperiodicity. During the epochs of aperiodic dynamics, the presence of defects makes the oscillators contribute destructively to  $p(t)$ .

Finally, for  $\gamma = 0.0038$  as in figure 1(h), the upper bound  $|p| = p_{\max}$  is attained periodically, because defects have been fully suppressed by the positive global coupling leading to the complete synchronization of all oscillators. Thus, all oscillators contribute constructively to the integrand in equation (4) when at maximum amplitude. In this way, our theory elucidates the emergence of OI. We conclude that, the transition from low-amplitude aperiodic oscillations to large-amplitude periodic ones via the route of intermittency in  $p(t)$  is essentially a transition from a state of defect to phase turbulence in the GCGLE as a consequence of increase in linear global coupling.



The time series of  $p(t)$  in figures 1(e)–(h) derived from the mean-field behavior of GCGLE accurately replicate the dynamics of realistic time series data obtained from experiments in thermoacoustic, aero-acoustic and aeroelastic systems. To substantiate this statement, we now calculate the Hurst exponent  $H$  of  $p(t)$  for an ensemble of 3000 simulations of our model at different  $\gamma$  values in the interval  $0 \leq \gamma \leq 0.0038$ . Generally,  $H$  has values between 0 and 1 for time series (i.e. a fractal dimension between 1 and 2), and provides a measure of persistence [36]. An antipersistent signal has  $H < 0.5$ , in which a high value of the signal is most likely followed by a low value, whereas for a persistent signal  $H > 0.5$ . Note,  $H = 0.5$  corresponds to an uncorrelated random process [15].

The Hurst exponent  $H$  is used to predict the onset of OI in experimental systems [15].  $H$  quantifies the scaling of the root mean squared (rms) of the standard deviation of fluctuations with the scale size or the time interval considered for obtaining the fluctuations. Recently, it was reported that the amplitude  $A$  of the dominant mode of oscillations increases and follows a universal scaling law  $A \propto H^{-2.0 \pm 0.2}$  [15]. A spectral measure  $\mu$ , which quantifies the sharpening of peaks in the power spectrum as the system dynamics approaches OI, has also been introduced and another universal scaling law  $A \propto \mu^{-0.66 \pm 0.10}$  [37, 38] has been discovered. In both cases, the scaling exponents are invariant across aero-acoustic, thermoacoustic and aeroelastic systems.

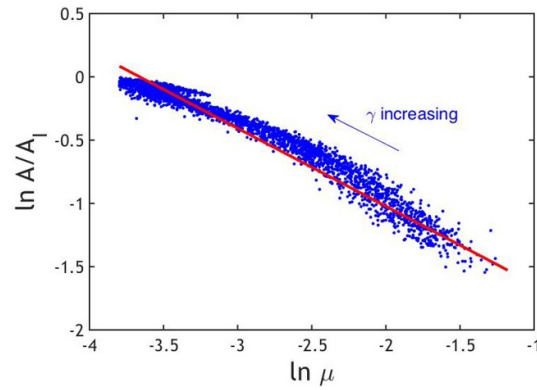
In figure 2, the logarithm of the normalized amplitude of the dominant Fourier mode  $A/A_I$  is plotted as a function of the logarithm of  $H$  for the ensemble of time series obtained with our model. As  $\gamma$  is increased, the Hurst exponent decreases and the amplitude of the dominant mode increases until the dominant mode coincides with the mode of the uniform synchronous oscillation. We find that the scaling relationship obtained from our model is  $A/A_I \propto H^{-2.0 \pm 0.1}$ , which is in excellent agreement with the experimental results from fluid mechanical systems [15].

Furthermore, a transition of power spectra from a broad peak to a sharp one is obtained as the onset of the OI is approached [37]. Spectral measures which quantify the sharpening of peaks in the power spectrum have been introduced. They are calculated as the product of different moments of the normalized power spectrum raised to integer powers, and they follow inverse power law relations with the corresponding peak power [37]. The most prominent spectral measure  $\mu$  is defined as

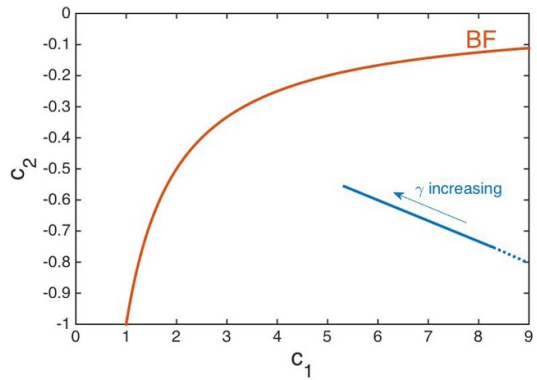
$$\mu := \left[ \int_{-\delta F}^{\delta F} \frac{P(F)}{P_0} \left| \frac{F}{f_0} \right|^2 dF \right] \times \left[ \int_{-\delta F}^{\delta F} \frac{P(F)}{P_0} dF \right]. \quad (7)$$

Here  $P(F)$  is the power corresponding to the modified frequency  $F = f - f_0$ , where  $f$  indicates the frequency of oscillations,  $f_0$  is the frequency corresponding to the dominant peak in the power spectrum, and  $P_0 := P(f_0)$ . A universal scaling relationship relating the normalized amplitude  $A/A_I$  of the dominant mode of oscillations and the spectral measure  $\mu$  has been obtained from experiments as  $A \propto \mu^{-0.66 \pm 0.10}$  [37]. In figure 3 the normalized amplitude of the dominant Fourier mode is plotted as a function of the spectral measure  $\mu$  for the ensemble of time series obtained from the GCGLE model (equations (1)–(3)). The scaling relationship  $A/A_I \propto \mu^{-0.61 \pm 0.04}$  is retrieved, also in excellent agreement with the scaling relationship obtained from experiments.

Figure 4 shows the location of the  $(c_1, c_2)$  pairs obtained from equations (2) and (3) in the  $c_2 - c_1$  plane as  $\gamma$  is varied. The continuous blue line shows the  $(c_1, c_2)$  pairs when  $\gamma$  is varied between 0 to 0.0038 and by a



**Figure 3.** Normalized amplitude of the dominant Fourier mode plotted as a function of the spectral measure  $\mu$  for the 3000 time series obtained from equations (1) to (3) and used in figure 2. The scaling relationship  $A/A_1 \propto \mu^{-0.61 \pm 0.04}$  is obtained (red line). The decreasing value of the spectral measure  $\mu$  as the global coupling parameter  $\gamma$  is increased, leads to a sharpening of the peaks in the Fourier spectrum of the time-series of the pressure indicating the onset of the OI.



**Figure 4.** Location in the  $c_2 - c_1$  plane of the parameter values obtained from equations (2) and (3) as  $\gamma$  is varied from 0 to 0.0038 (continuous blue line) and for  $\gamma$  negative (dotted line). This path in parameter plane leads to the theoretical universal scaling relationships shown in figures 2 and 3 which accurately reproduce those found in the experiments. Also, the Benjamin–Feir (BF) line is shown.

dotted line for  $\gamma < 0$ . All  $(c_1, c_2)$  pairs fall in a region in the plane where the uniform oscillation is unstable when the GCGLE without global coupling is considered. The effect of a positive global coupling in our model is twofold: 1) it tends to suppress turbulence and 2) it displaces the values of  $c_1$  and  $c_2$  closer to the BF line (also shown in figure 4). The latter also has a stabilizing effect, since it removes unstable Fourier modes out of the turbulent patterns. These two effects are directly responsible for the behavior observed in the spectral measure in figure 3 as the global coupling is increased.

The fixed parameter values entering equations (2) and (3) have been found through an extensive and systematic search of the parameter space. Although spatiotemporal chaos and intermittency exist outside the region of turbulence bounded by the BF line [33], computational evidence suggests that the scaling relationships in figures 2 and 3 are nowhere else to be found in the parameter plane.

#### 4. Conclusion

In this work, we propose a globally coupled complex Ginzburg Landau equation for modeling the transition from chaotic to periodic temporal dynamics in turbulent thermoacoustic, aero-acoustic and aeroelastic systems as found in experiments. The model arises from a center manifold reduction of the complex oscillatory spatiotemporal dynamics exhibited by many turbulent fluid and thermo-fluid systems close to an oscillatory instability which involves nonlinear interactions between hydrodynamic and acoustic modes and combustion dynamics or elasticity fields. Our model leads to an interpretation of the emergence of OI as a transition from defect to phase turbulence as the global coupling increases. Importantly, the universal scaling relationships discovered in experiments are accurately reproduced by our theory, and, therefore, the model is able to realistically replicate time series obtained from a wide variety of turbulent fluid mechanical systems.

## Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

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